



 POLITECNICO DI MILANO



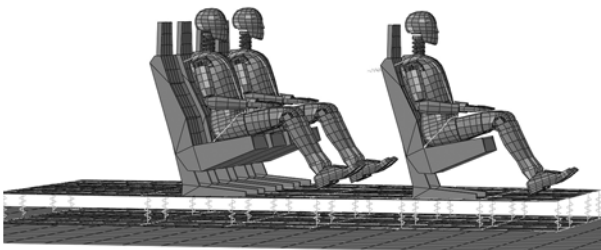
A Preliminary Study on Helicopter Crashworthy Stages Adapted to Different Impact Conditions

Paolo Astori

Department of Aerospace Science and Technology

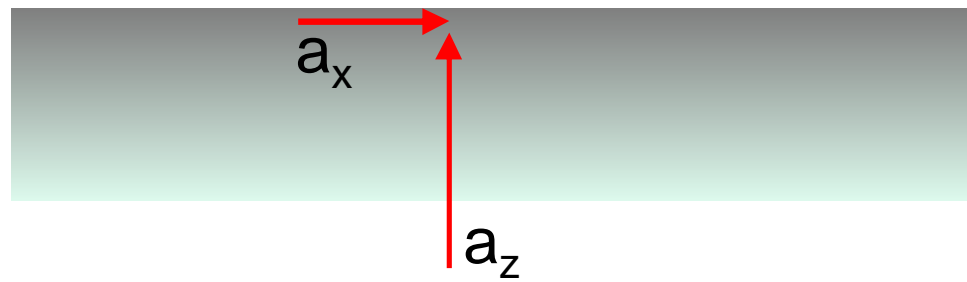


Crash and dynamic test facilities and numerical tools





High vertical component of acceleration



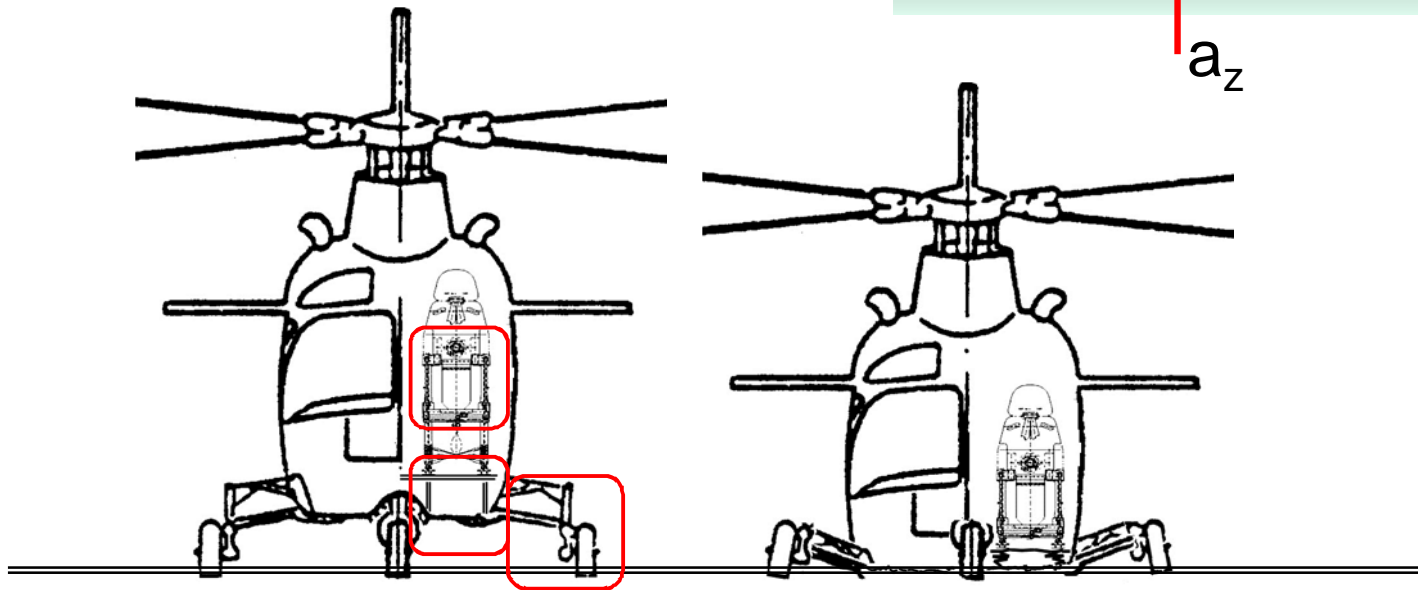
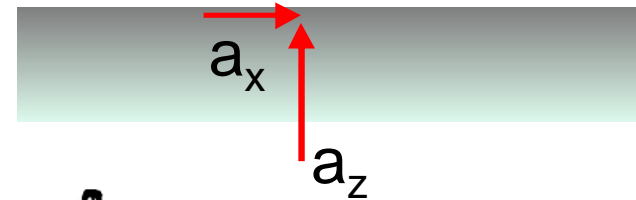
Main injury risk:

- High lumbar spine load



Energy absorption by:

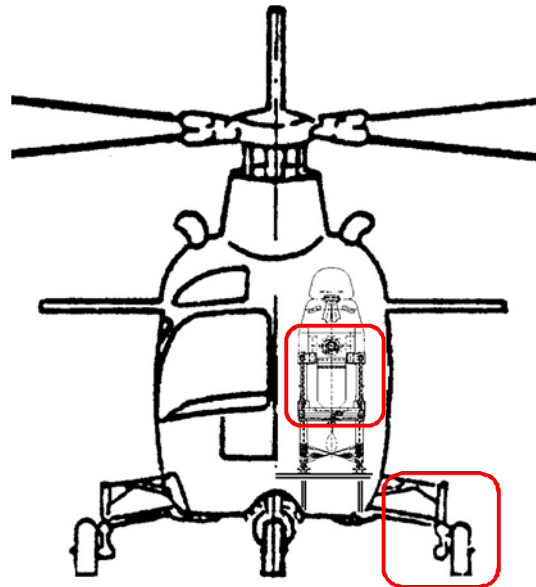
- Landing gear shock absorber (certification at $v = 2$ m/s)
- Subfloor (general recommendations)
- Seat (certification at 9.15 m/s, 30 g's)





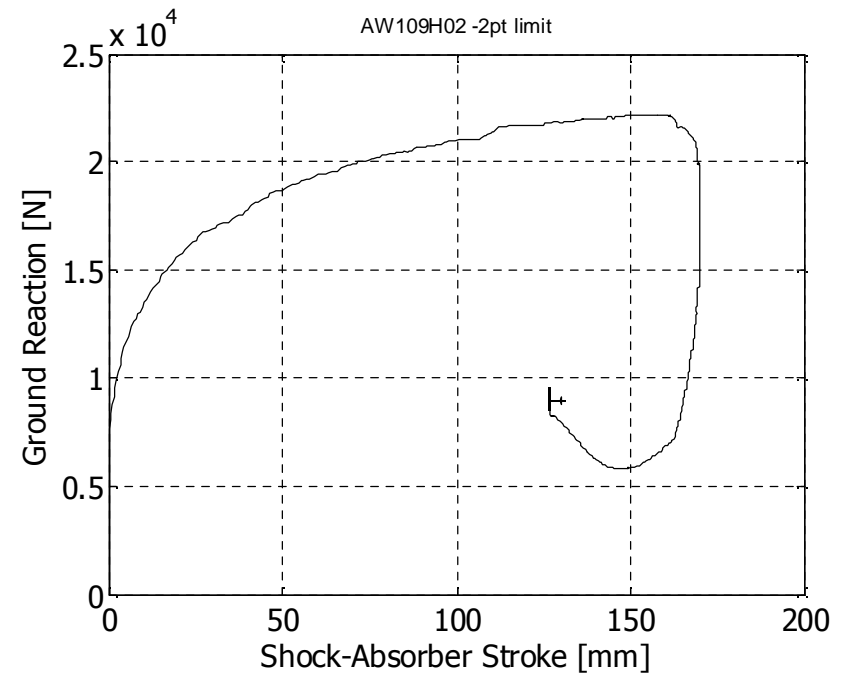
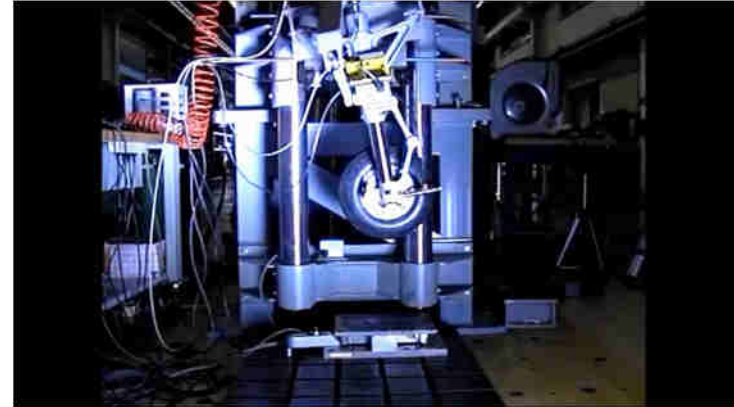
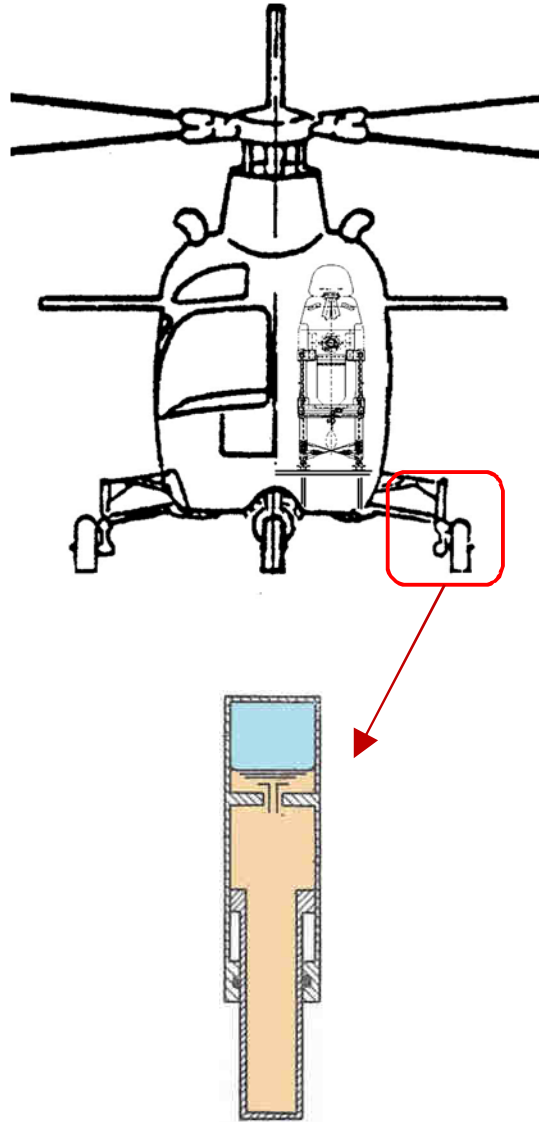
Preliminary study:

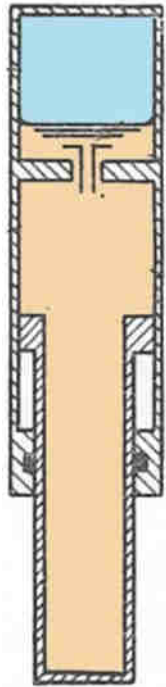
1. Set-up a numerical model of the relevant structural area and systems
2. Define the mechanical parameters that could be controllable and adaptive
3. Carry out parametrical analyses at increasing impact speeds





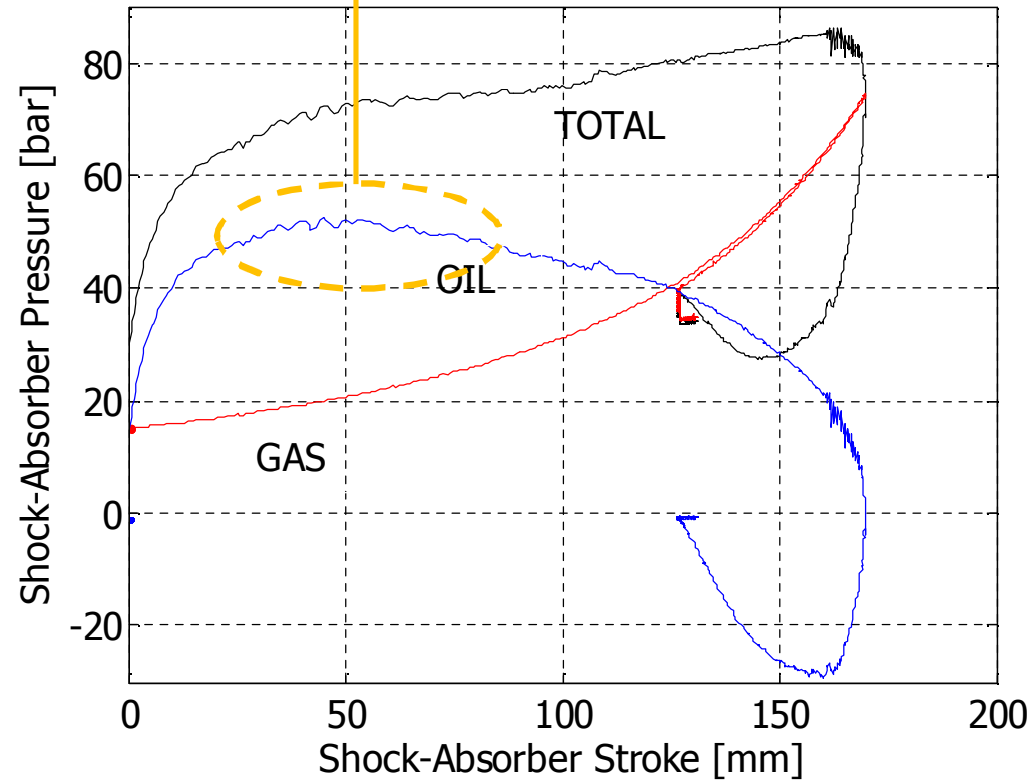
Landing gear





Increases with SA rate

AW109H02 -2pt limit



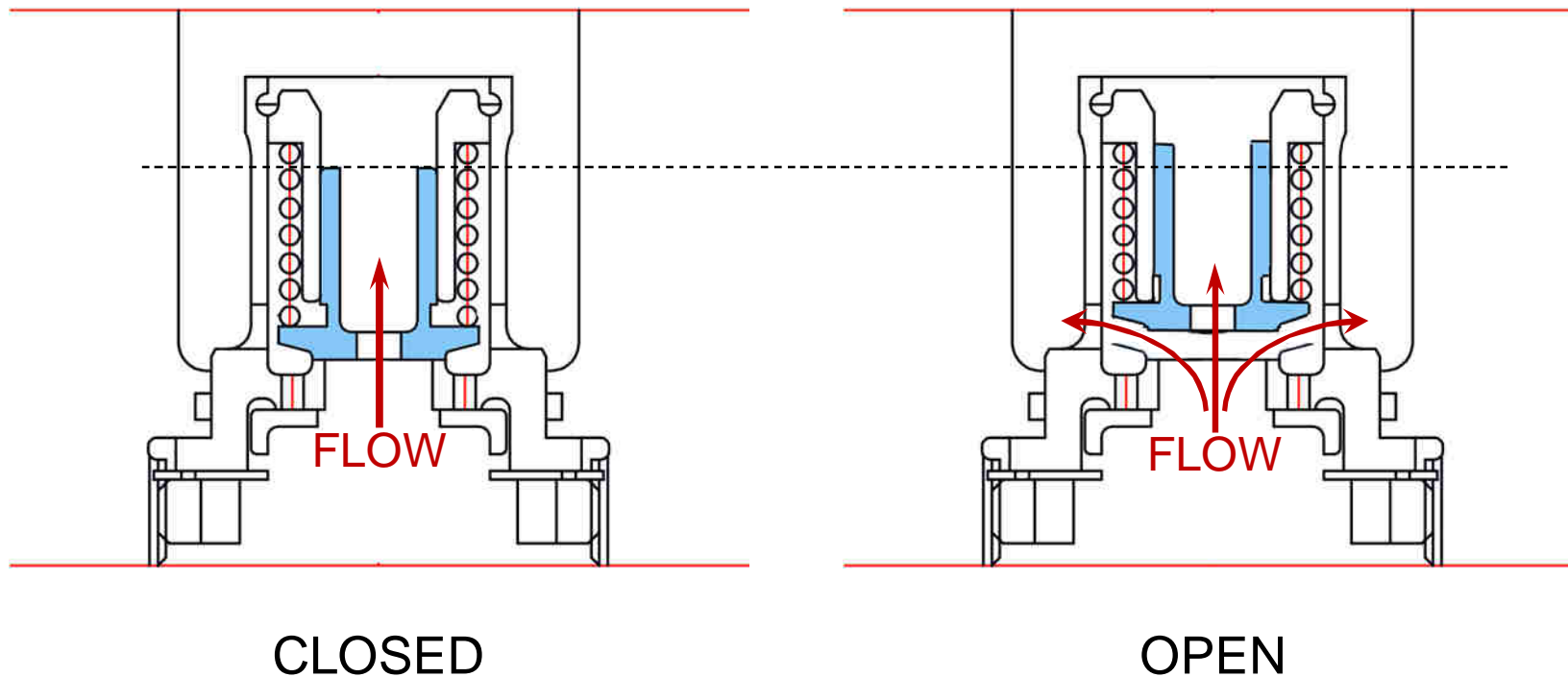


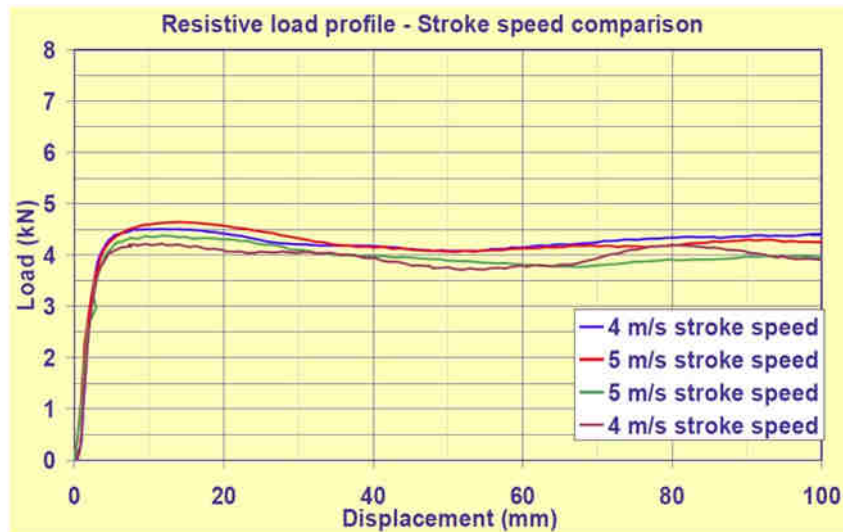
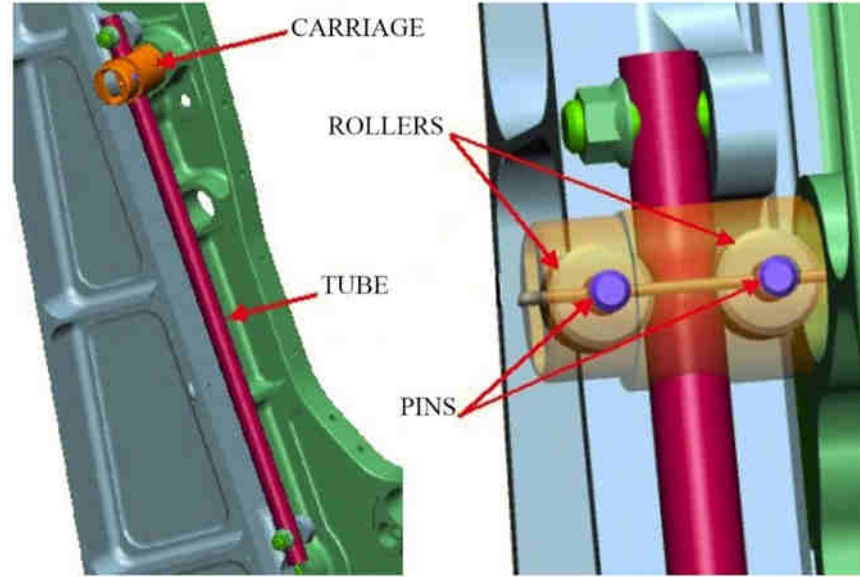
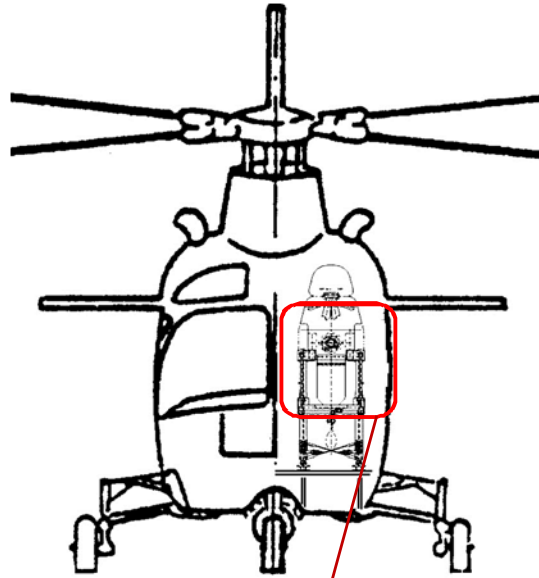
Adaptive shock absorber

Metering of the side orifice areas by electrically-controlled shutters

Control of max spool displacement

Magneto-rheological fluids

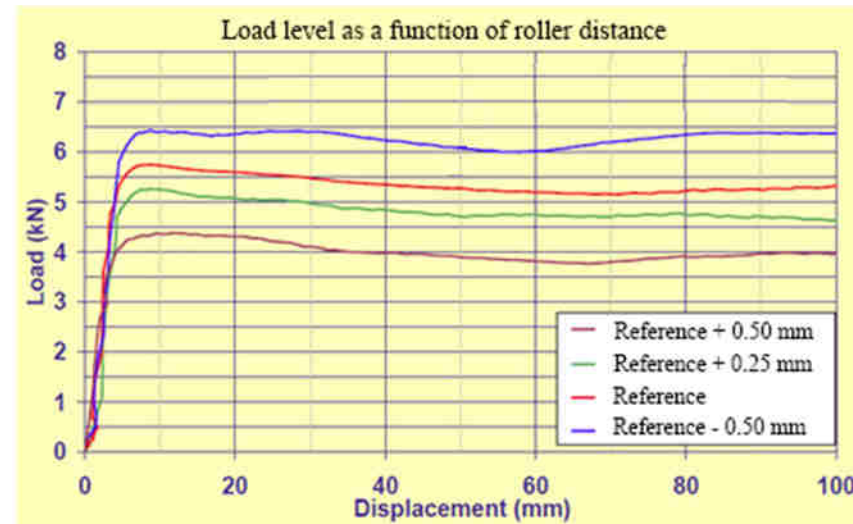
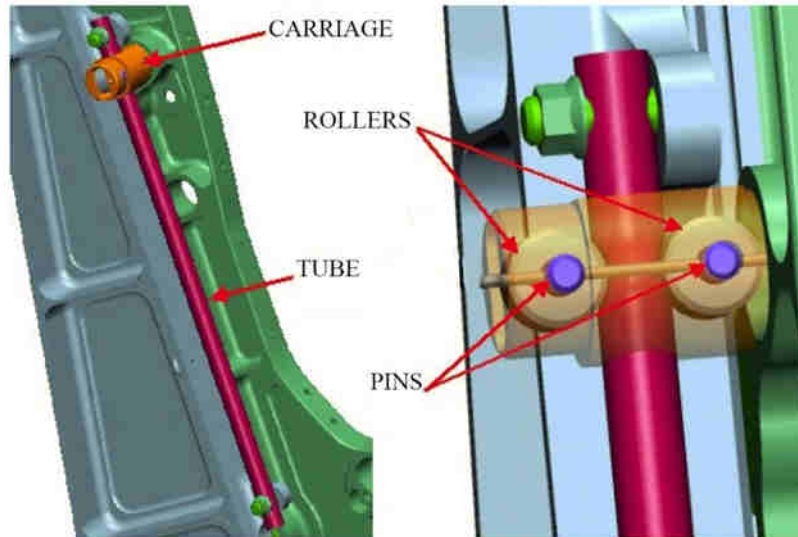
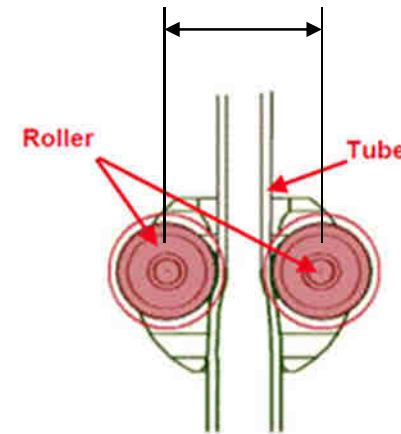






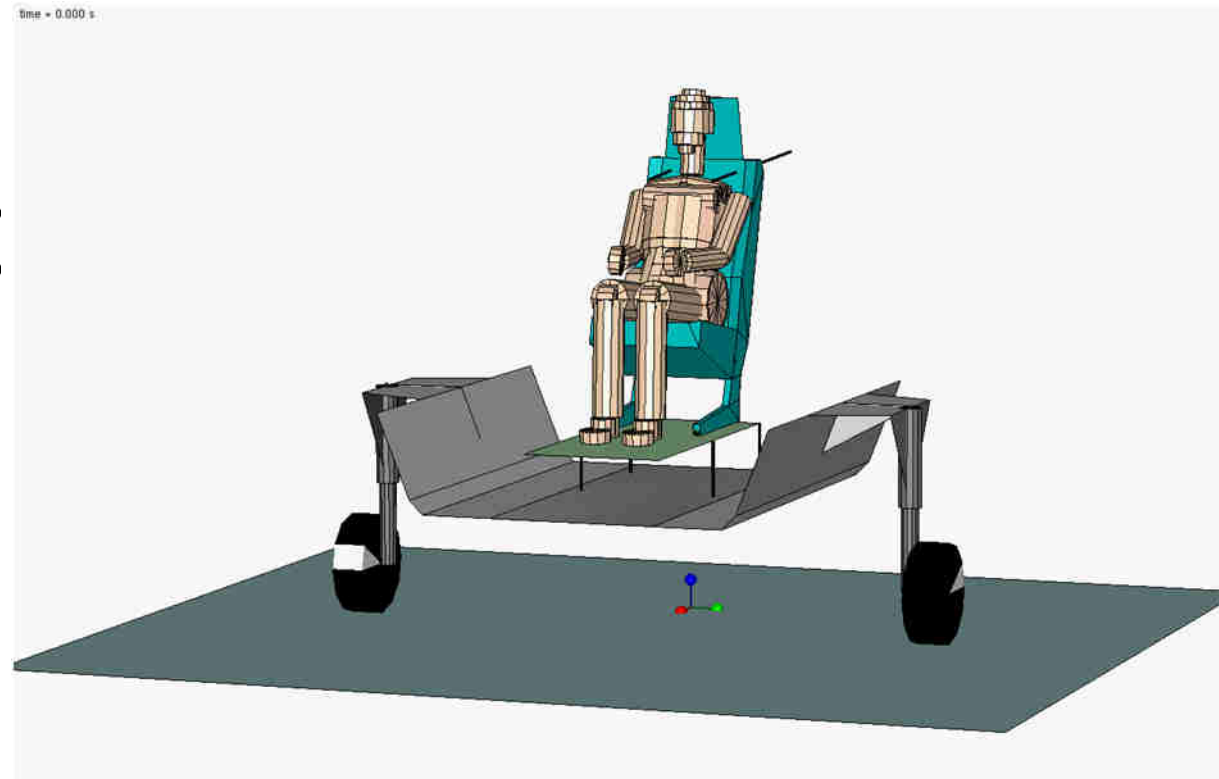
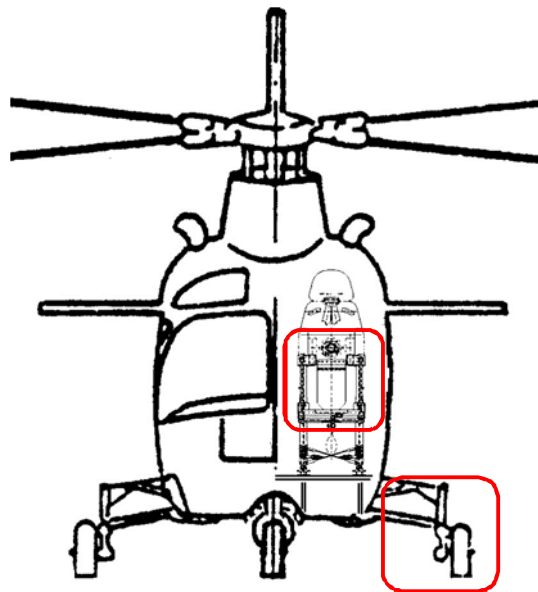
Adaptive energy absorber

Roller distance calibrated by a micro-actuation system





Simplified model based on lumped parameters approach
Anthropomorphic Test Dummy, Seat system and Landing Gear validated against experimental data in certification dynamic conditions





Sensitivity analysis - response surface:

- max lumbar spine loads as functions of the mechanical characteristics of landing gear shock absorber and seat energy absorber

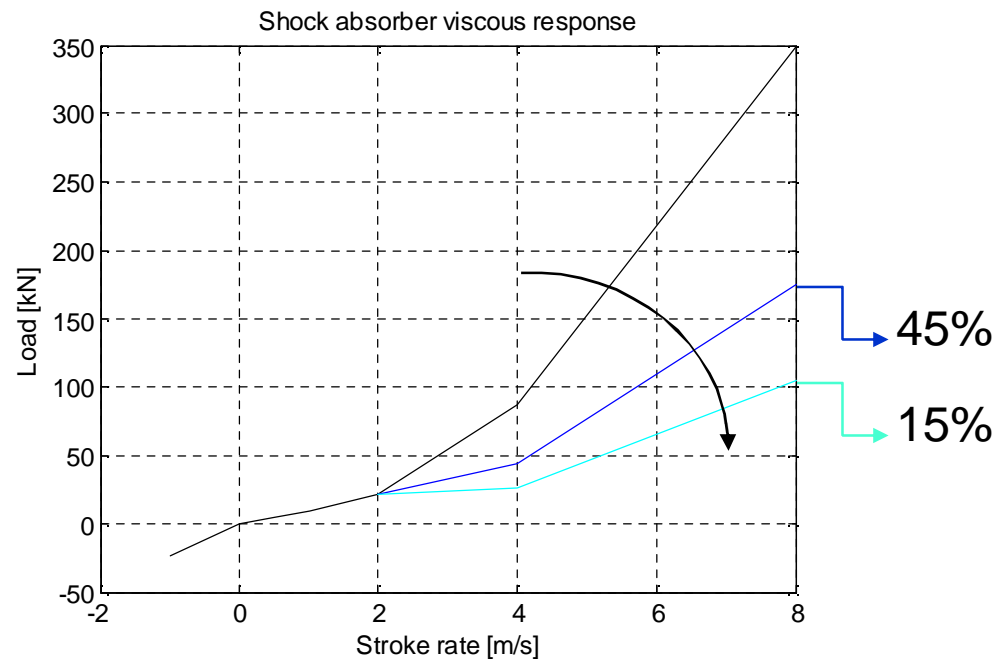
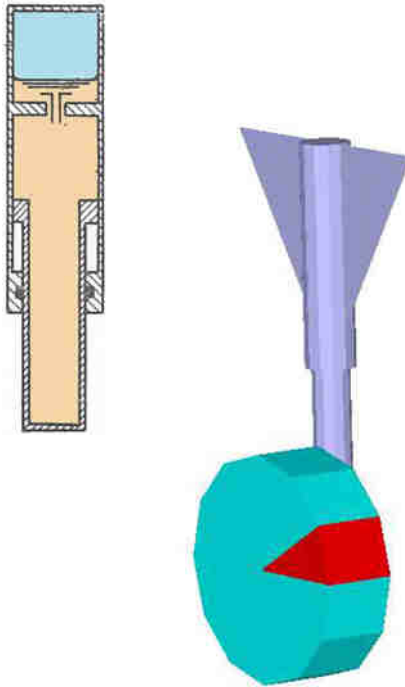


Landing gear

3 rigid bodies: wheel, piston block and cylinder block

Polytropic response: fixed

Viscous response: from 0 to 2 m/s from experimental data
from 2 to 4 m/s extrapolated but fixed
from 4 to 8 m/s variable

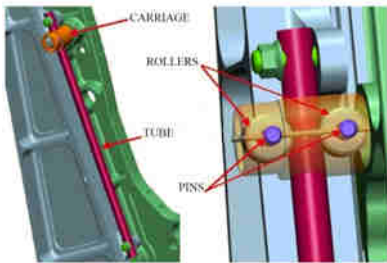




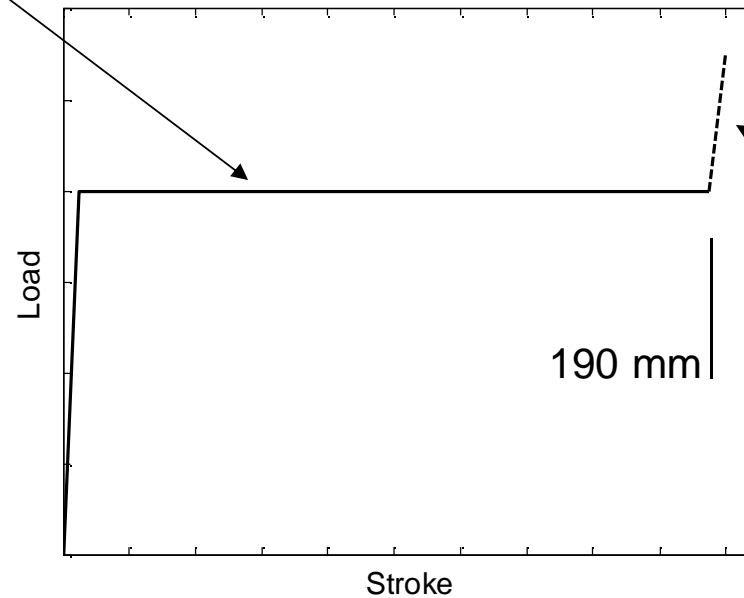
Seat energy absorber

2 rigid bodies: lower fixed part and upper moveable part

Elastic – perfectly plastic response



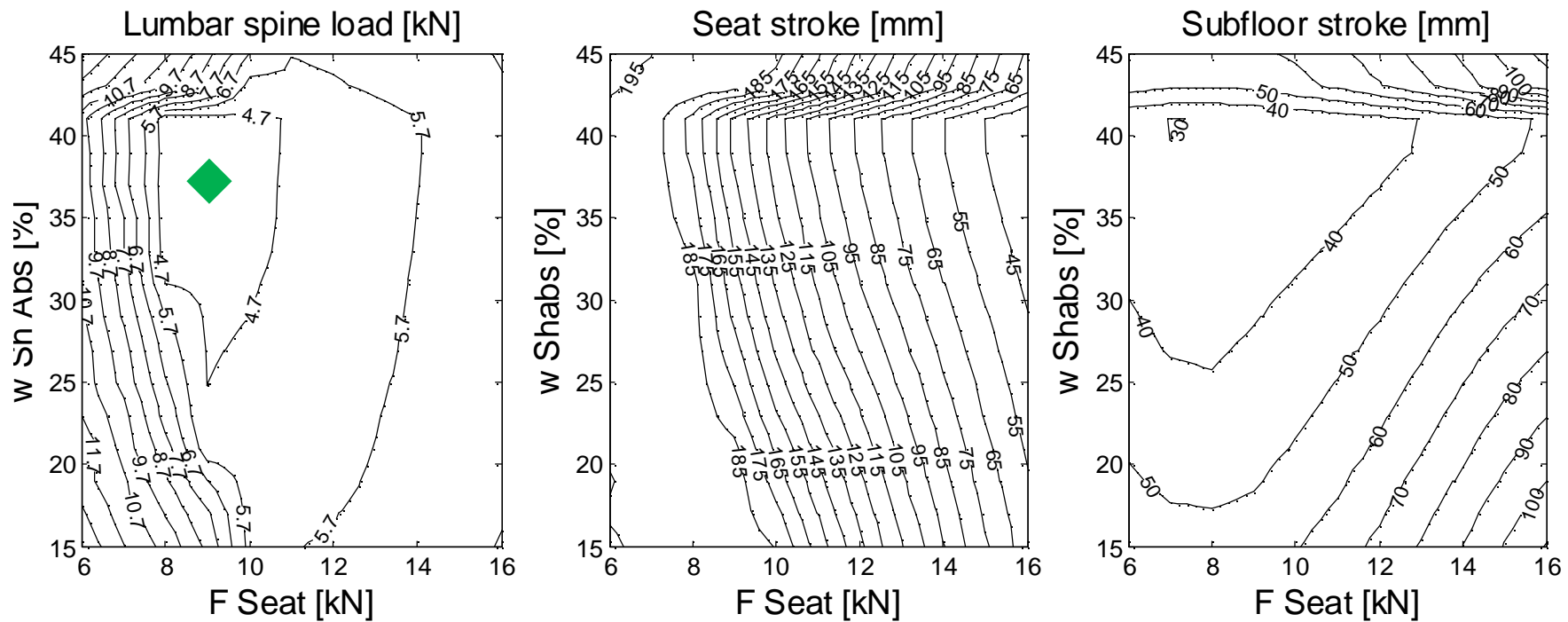
LOAD LEVEL RANGE: 6000 TO 16000 N



BOTTOMING



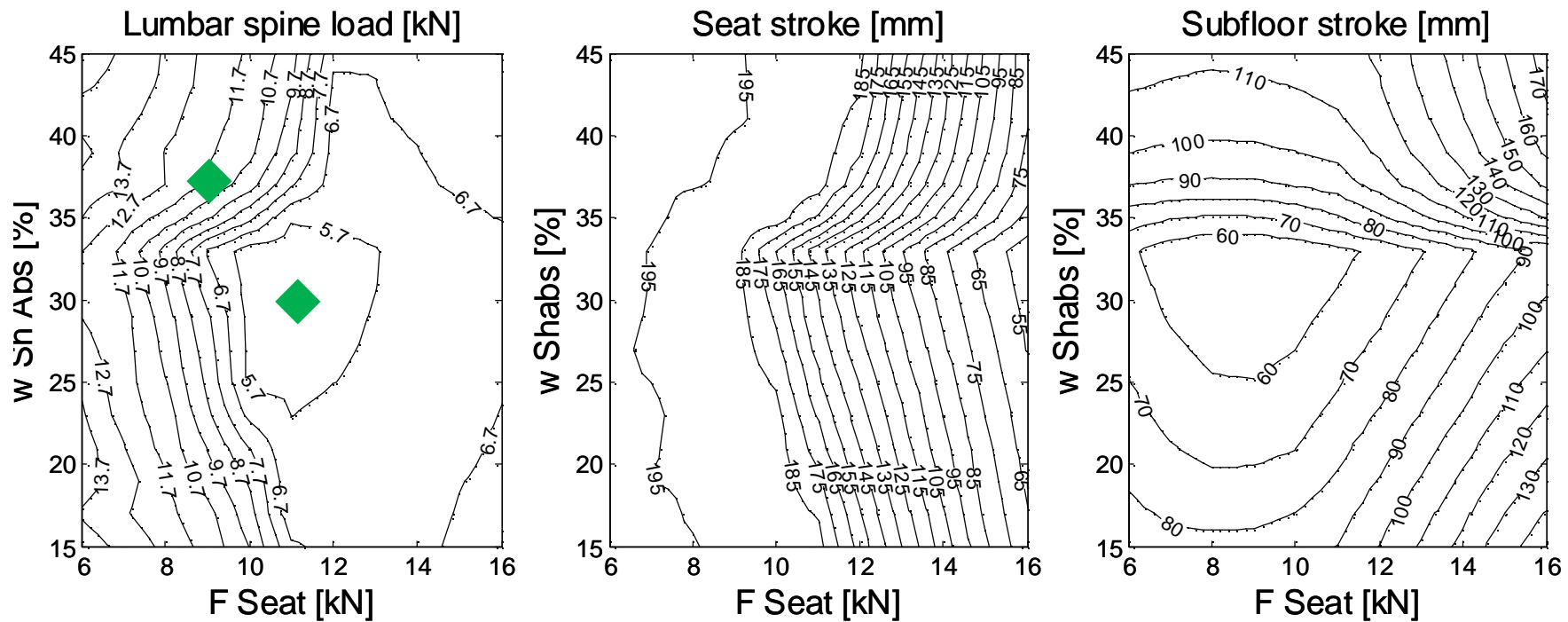
Response surfaces vs. impact speed from 11 to 15 m/s (std speed for seats $v = 9.15$ m/s)



11 m/s



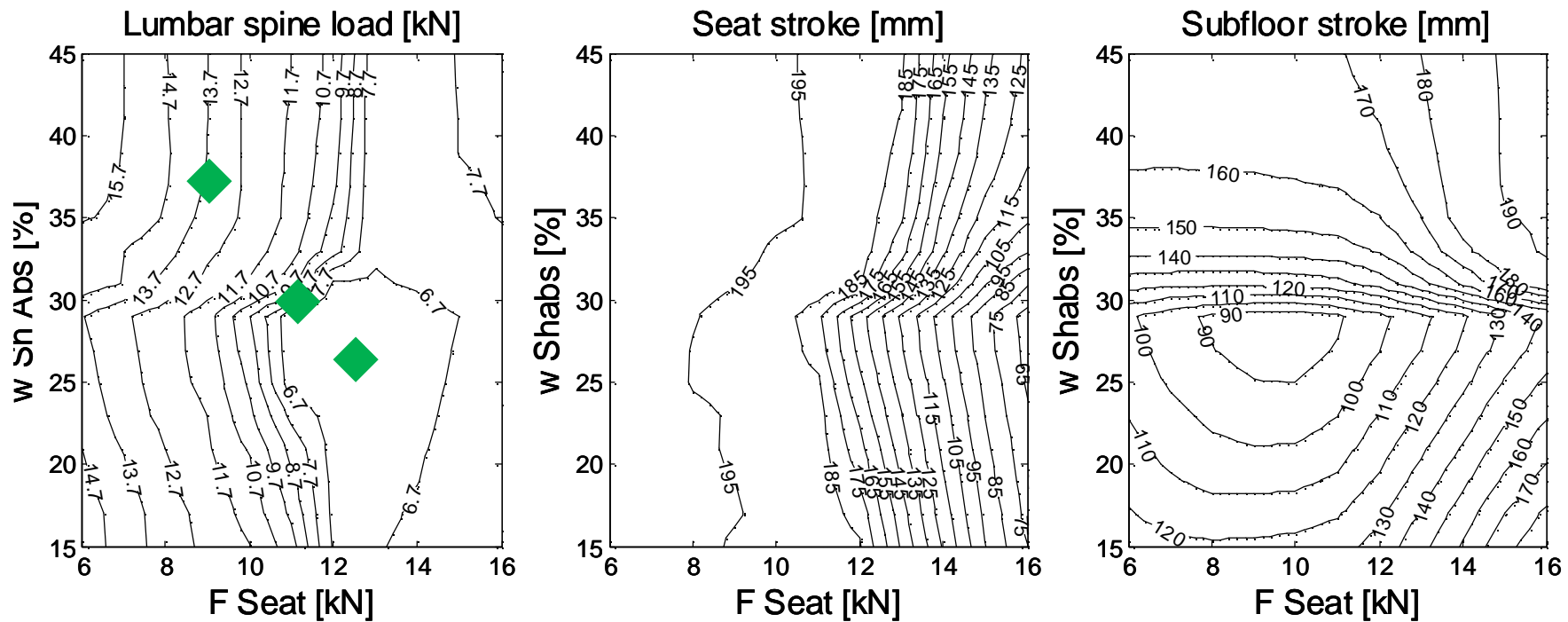
Response surfaces vs. impact speed from 11 to 15 m/s (std speed for seats $v = 9.15$ m/s)



12 m/s



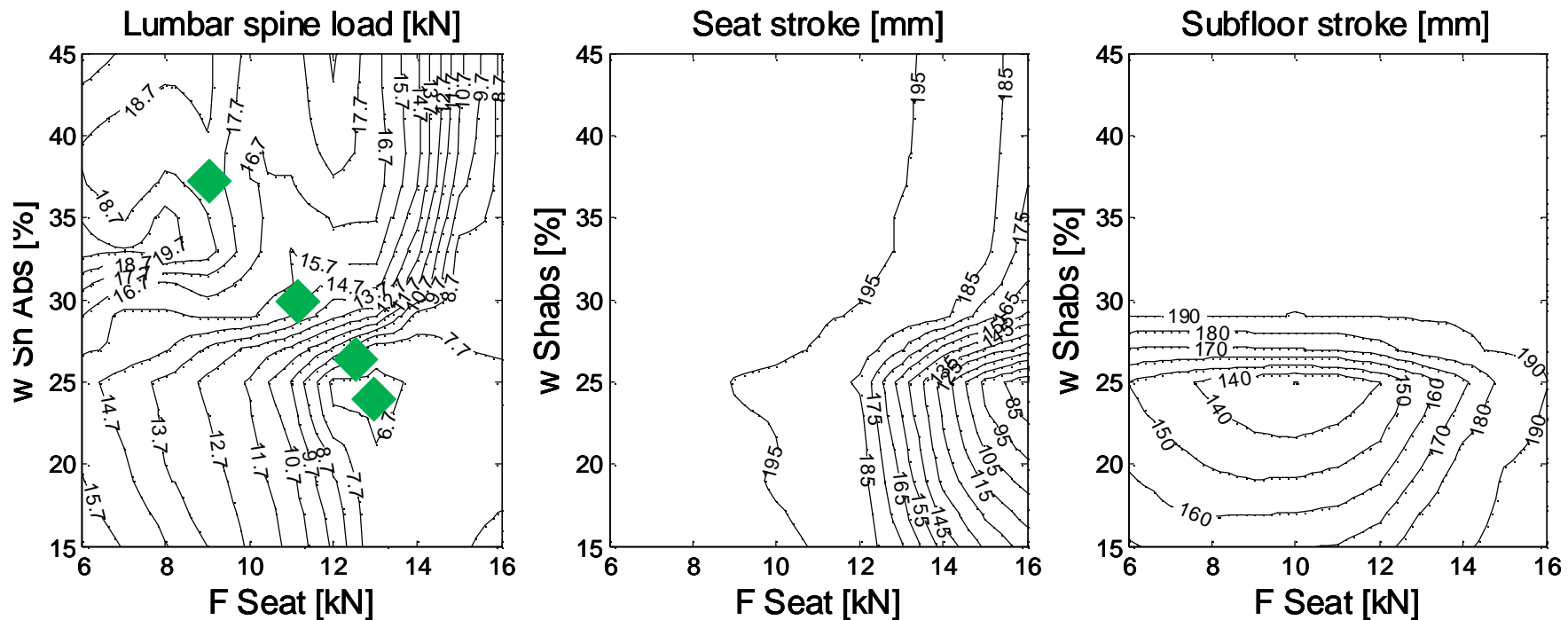
Response surfaces vs. impact speed from 11 to 15 m/s (std speed for seats $v = 9.15$ m/s)



13 m/s



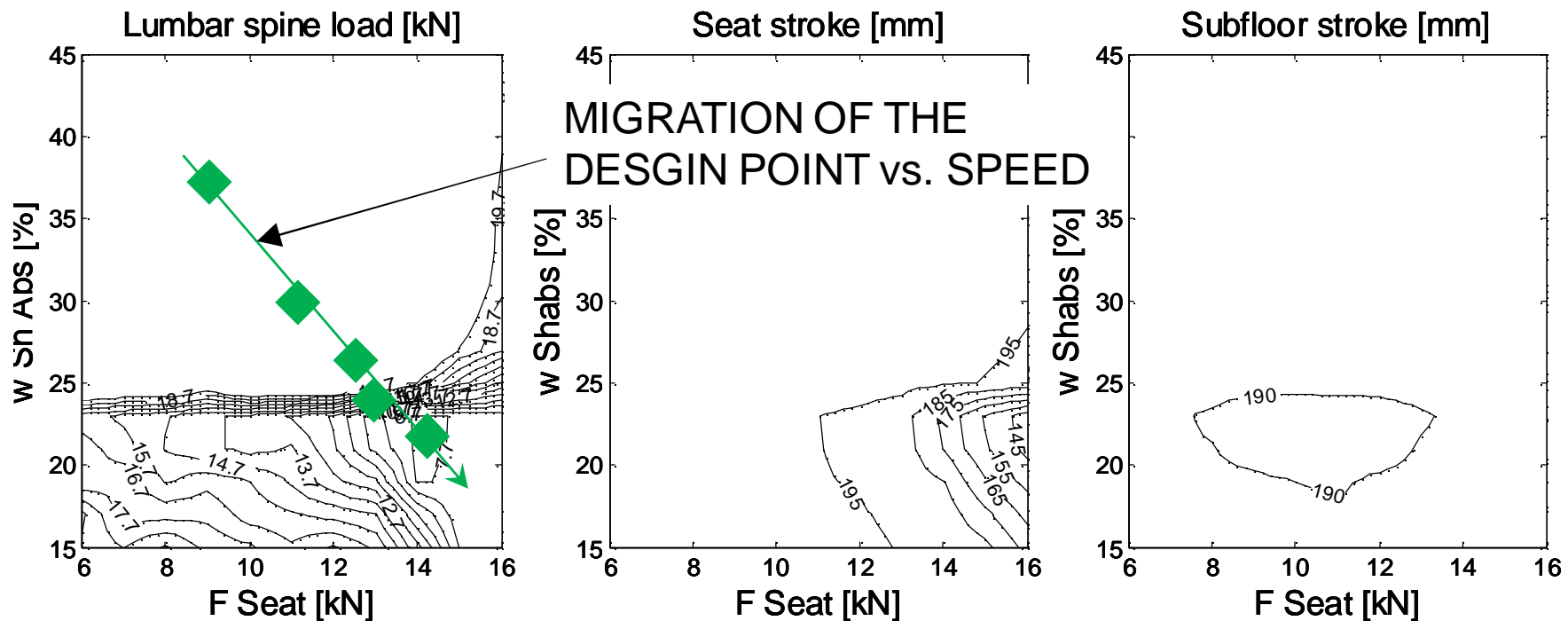
Response surfaces vs. impact speed from 11 to 15 m/s (std speed for seats $v = 9.15$ m/s)



14 m/s



Response surfaces vs. impact speed from 11 to 15 m/s (std speed for seats $v = 9.15$ m/s)



15 m/s



Crash landing condition triggered by ground proximity and vertical velocity detection



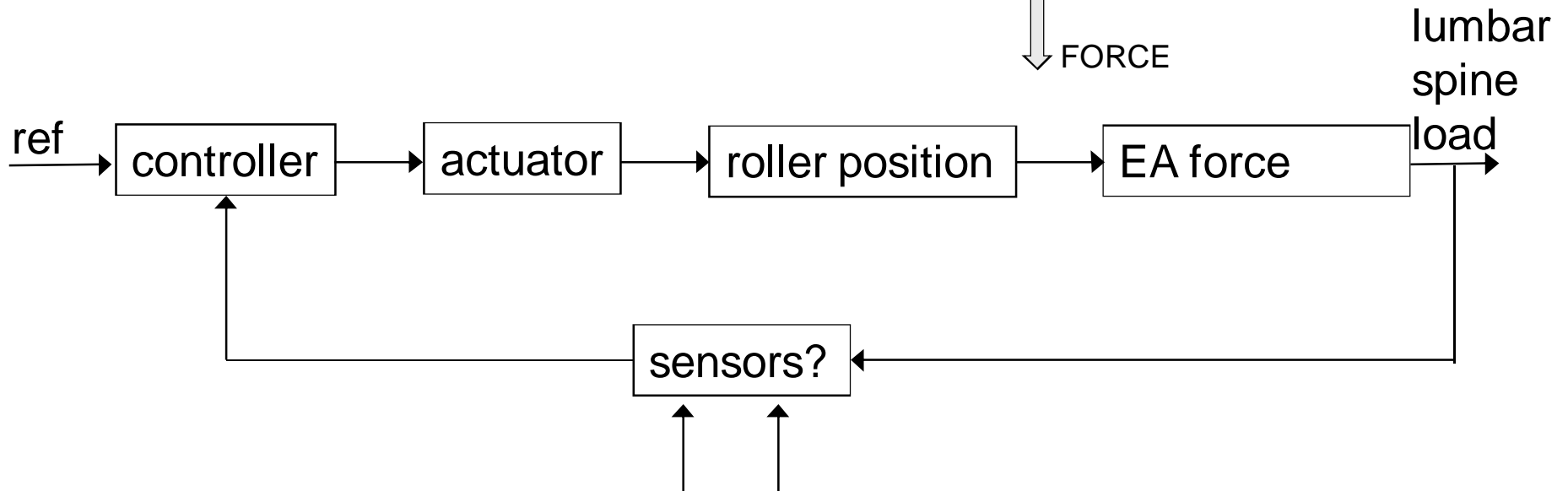
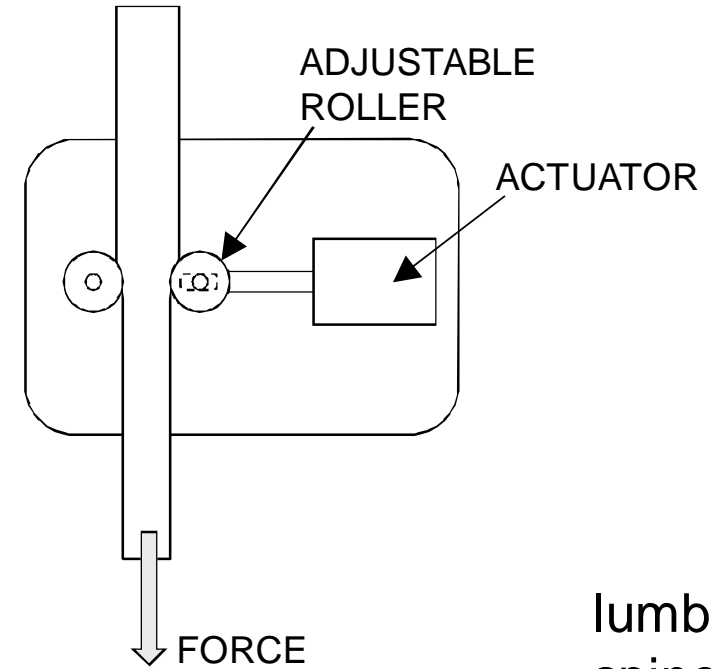
Pre-setting of landing gear shock absorber and seat energy absorber as a function of velocity (and occupant weight)

or

Closed-loop control?



Test rig for adaptive seat energy absorber





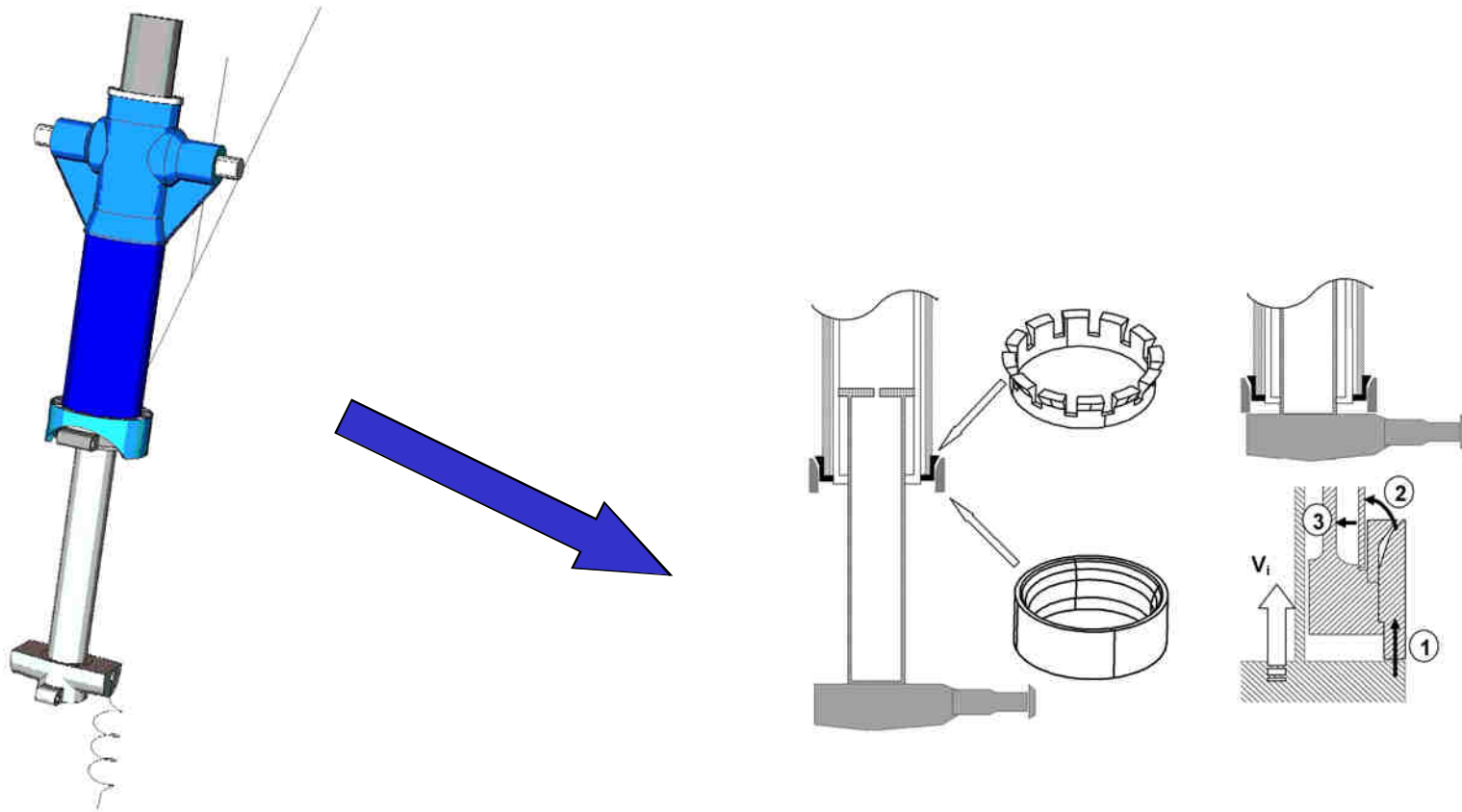


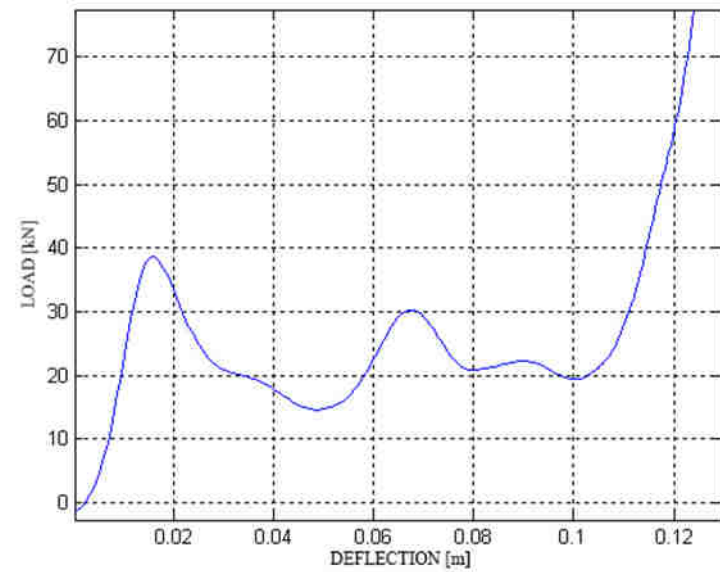
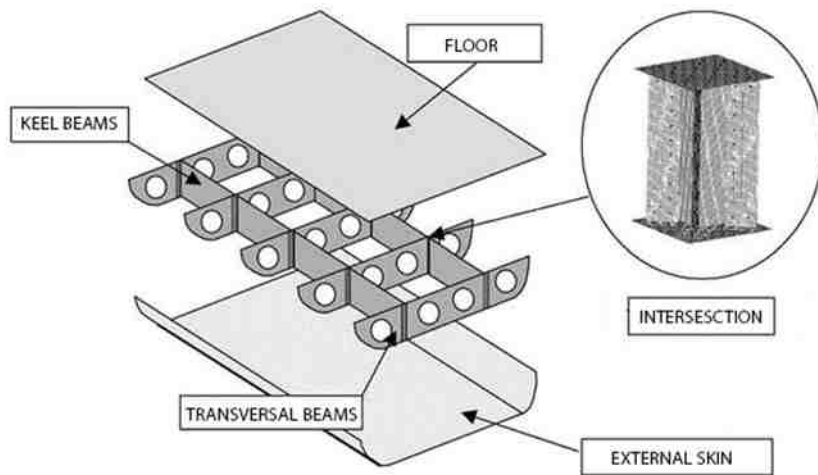
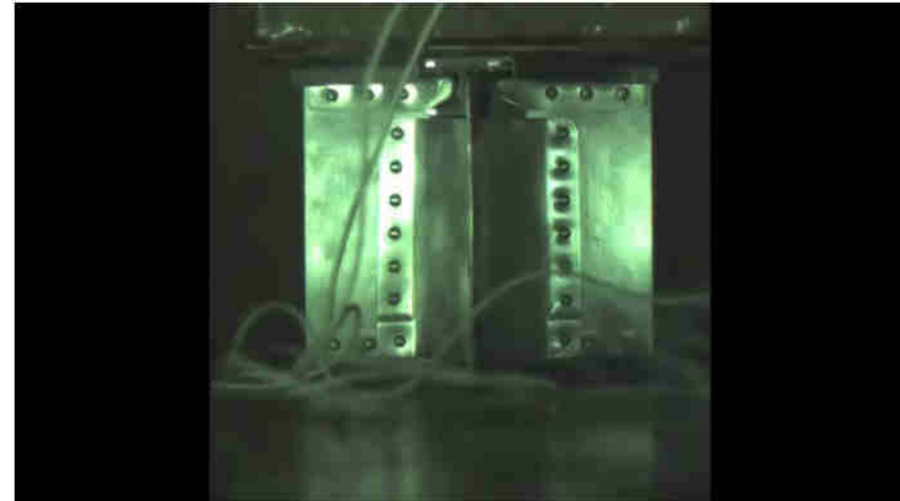
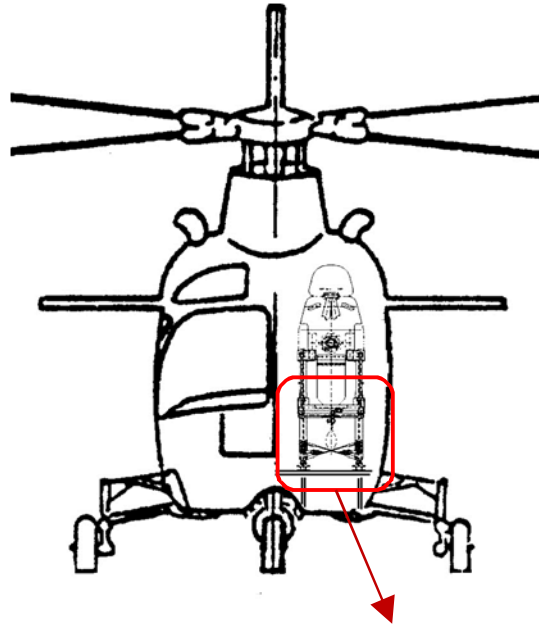
Helisafe TA EU project, full scale UH-1 crash test, 15 m/s, 32°





Introduction of a passive crash stage







Subfloor

1 rigid body: floor

Elastic – perfectly plastic response

Mechanical structure made of joined components \Rightarrow adaptive system hardly feasible

CRUSHING LOAD FIXED TO 6000 N (OPTIMUM IN HIGH SPEED CONDITION)

